

# Computational perspectives to hydrogen combustion using open-source code

Physics/chemistry views

Hydrogen Breakfast Seminar 4, Wednesday, May 29<sup>th</sup> 2024  
Otaniemi, Espoo



Associate Prof. Ville Vuorinen  
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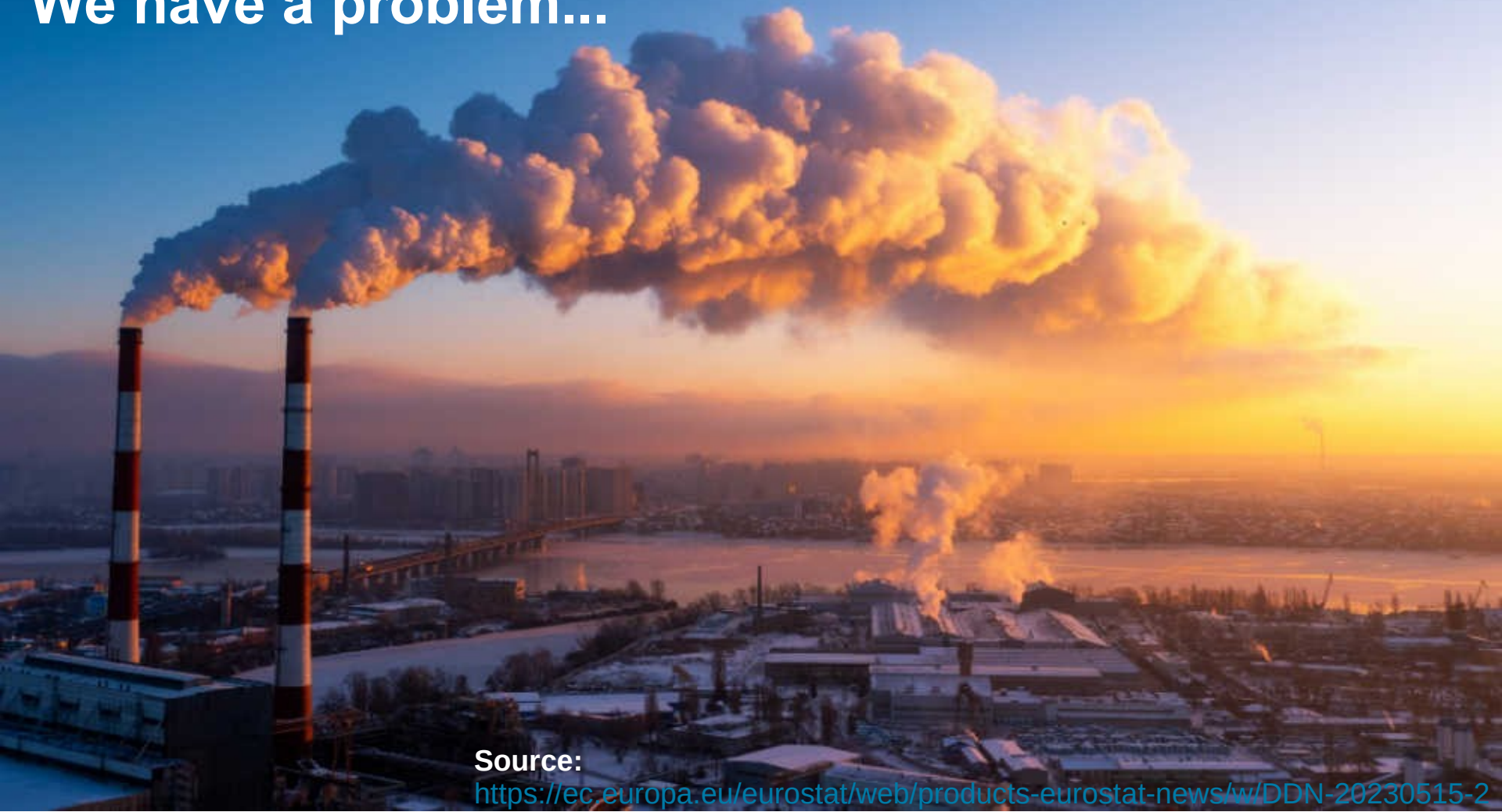
Fig: I. Morev

# Contents of the talk

- 1) Motivation
- 2) Computational fluid dynamics at Aalto/ENG in 2024
- 3) Remarks about hydrogen
- 4) Aalto/ENG + international efforts to model hydrogen flames
- 5) Concluding remarks

# 1) Motivation

# We have a problem...



Source:

<https://ec.europa.eu/eurostat/web/products-eurostat-news/w/DDN-20230515-2>

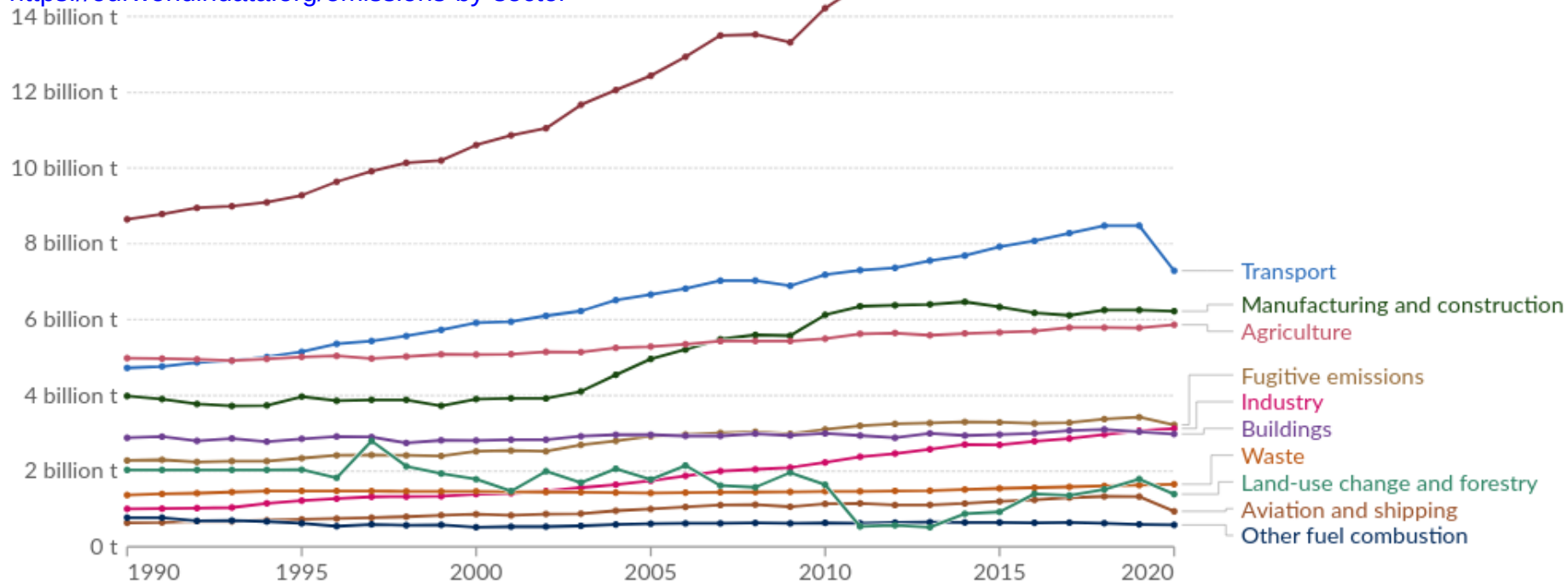


# Green house gas emissions by sector

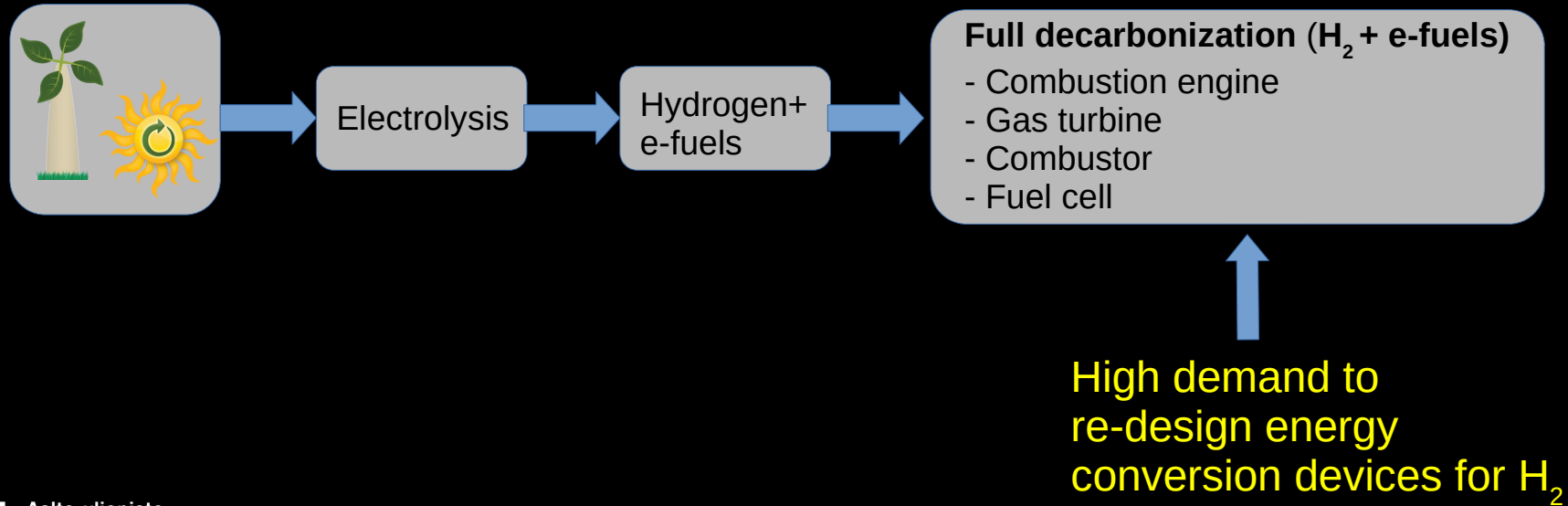
Measured in terms of CO2-equivalents over 100 year span

Source:

<https://ourworldindata.org/emissions-by-sector>



**Extreme vision:** there would be a great potential to even full decarbonization i.e. replacement of fossil fuels with hydrogen + e-fuels



# Example: combined heat and power (CHP) plants

CHP (80-90% eff.)



Heating/  
cooling

Electricity

Combustion device (e.g. engine)



Copyright Wärtsilä

CFD direct numerical simulation of reactive flow in gas engine cylinder by HPC (high-performance comp.)



Credit: George Giannakopoulos

$$\vec{U} = \vec{U}(x, y, z, t)$$
$$T = T(x, y, z, t)$$

$$\rho = \rho(x, y, z, t)$$
$$p = p(T)$$

# Example: combined heat and power (CHP) plants

CHP (80-90% eff.)



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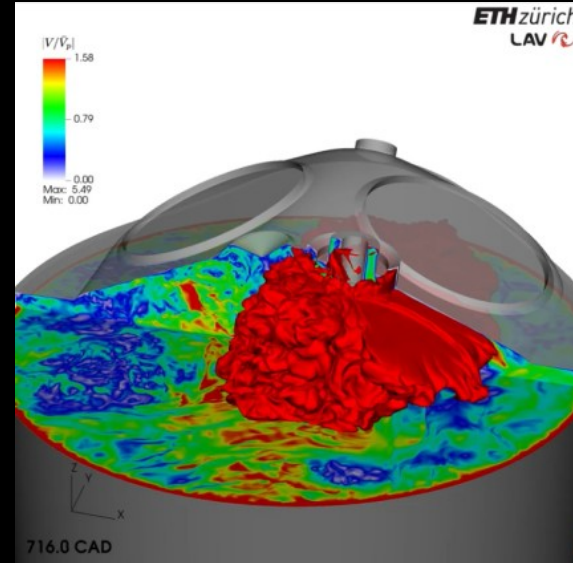
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$$\rho = \rho(x, y, z, t)$$
$$p = \rho R T$$

# HPC + CFD caveats

- CFD is computationally quite heavy
- Requires HPC i.e. either a cluster or a supercomputer
- CFD requires highly educated/experienced users
- CFD of reactive flows extremely heavy
- CFD of reactive flows highly multidisciplinary: engineering + physics + chemistry + software + HPC + data management

## 2) Computational fluid dynamics at Aalto/ENG

## Computational fluid dynamics team at Aalto University/ENG, Finland

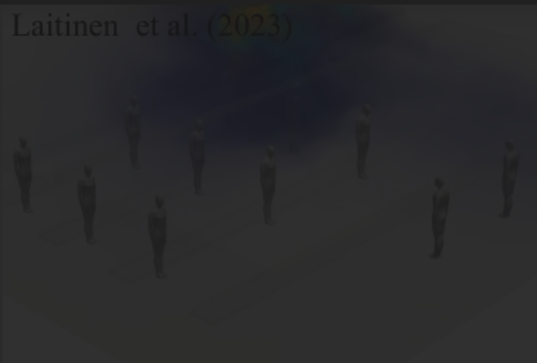
- Prof. V.Vuorinen + Prof. O.Kaario + 20 researchers
- 15 supervised PhD's, 100+ journal papers
- Hydrogen, e-fuels, reactive multiphase flow, heat transfer, gas-/hydrodynamics
- OpenFOAM, StarCCM+, STAR-CD, LES/DNS/RANS/DES, DLBFoam



### Wind power efficiency in landscapes



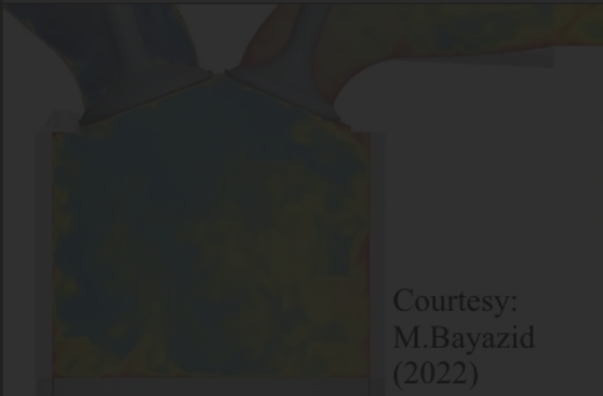
### Healthy indoor air/vertical farming



### Energy conversion to H2/burners



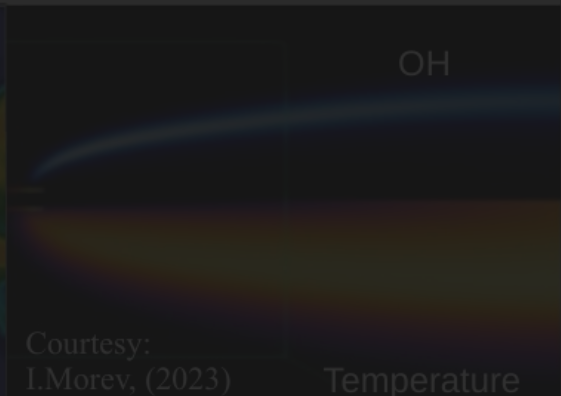
### Energy conversion to H2/engines



### Heat transfer and energy



### Hydrogen flame physics/chemistry



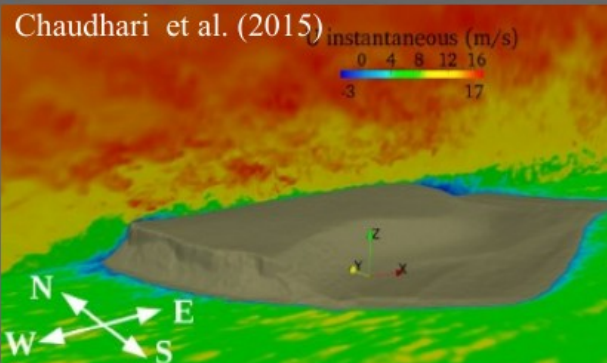


## Computational fluid dynamics team at Aalto University/ENG, Finland

- Prof. V.Vuorinen + Prof. O.Kaario + 20 researchers
- 15 supervised PhD's, 100+ journal papers
- Hydrogen, e-fuels, reactive multiphase flow, heat transfer, gas-/hydrodynamics
- OpenFOAM, StarCCM+, STAR-CD, LES/DNS/RANS/DES, DLBFoam



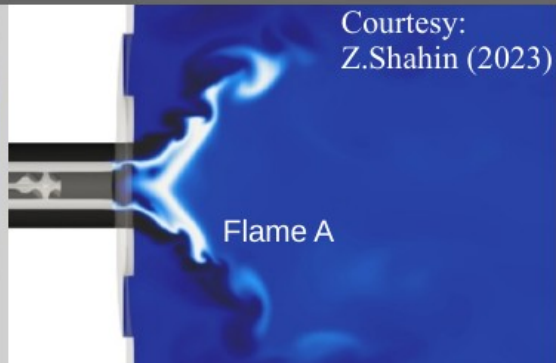
Wind power efficiency in landscapes



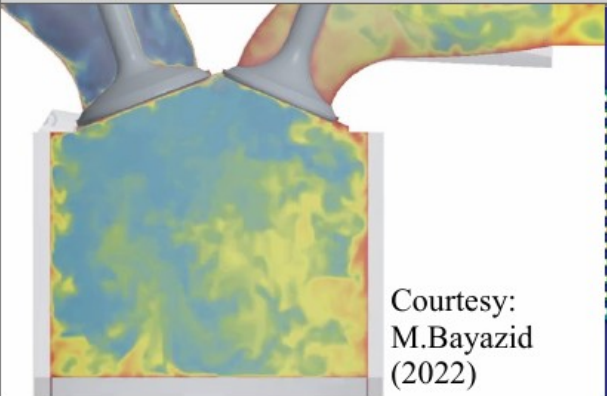
Healthy indoor air/vertical farming



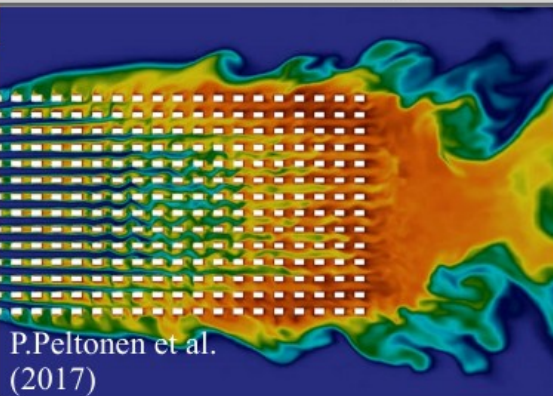
Energy conversion to H2/burners



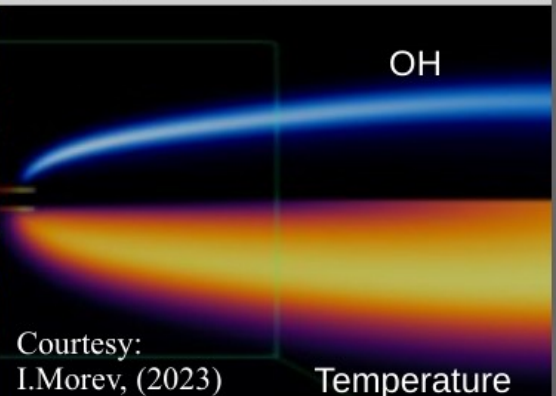
Energy conversion to H2/engines



Heat transfer and energy



Hydrogen flame physics/chemistry





# OpenFOAM: the world's largest open-source code for computational fluid dynamics (CFD)



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## OPENFOAM 11

FLUID SIMULATION  
SOLID FOUNDATION

<https://openfoam.org/11>



Read More



### OpenFOAM and The OpenFOAM Foundation

OpenFOAM is free, open source software for CFD from the OpenFOAM Foundation.

> OpenFOAM is the leading free, open source software for computational fluid dynamics (CFD)

> The OpenFOAM Foundation is the independent distributor of OpenFOAM

#### OpenFOAM Supporters

Gold Level (€25k+ per year)

The following organisations have purchased OpenFOAM Maintenance Plans to Gold level to fund OpenFOAM maintenance in 2024.



Silver Level (€5k-€25k per year)

The following organisations have purchased OpenFOAM Maintenance Plans to Silver level to fund OpenFOAM maintenance in 2024.



# Governing equations in reactive flow CFD simulation

$$\frac{\partial \bar{\rho}}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_i}{\partial x_i} = \bar{S}_\rho, \quad (1)$$

Mass conservation (1 eqn)

$$\frac{\partial (\bar{\rho} \tilde{u}_i)}{\partial t} + \frac{\partial (\bar{\rho} \tilde{u}_i \tilde{u}_j)}{\partial x_j} = \frac{\partial}{\partial x_j} (-\bar{p} \delta_{ij} + \bar{\rho} \tilde{u}_i \tilde{u}_j - \bar{\rho} \tilde{u}_i \tilde{u}_j + \bar{\tau}_{ij}) + \bar{S}_{u,i}, \quad (2)$$

Momentum conservation (3 eqs)

$$\frac{\partial (\bar{\rho} \tilde{Y}_k)}{\partial t} + \frac{\partial (\bar{\rho} \tilde{u}_i \tilde{Y}_k)}{\partial x_i} = \frac{\partial}{\partial x_i} \left( \bar{\rho} \tilde{u}_i \tilde{Y}_k - \bar{\rho} \tilde{u}_i \tilde{Y}_k + \bar{\rho} \tilde{D} \frac{\partial \tilde{Y}_k}{\partial x_i} \right) + \bar{S}_{Y_k} + \bar{\omega}_k, \quad (3)$$

Species conservation (~10-30 eqs for H<sub>2</sub>)

$\sim N_{\text{species}}$

$$\frac{\partial (\bar{\rho} \tilde{h}_t)}{\partial t} + \frac{\partial (\bar{\rho} \tilde{u}_j \tilde{h}_t)}{\partial x_j} = \frac{\partial \bar{p}}{\partial t} + \frac{\partial}{\partial x_j} \left( \bar{\rho} \tilde{u}_j \tilde{h}_s - \bar{\rho} \tilde{u}_j \tilde{h}_s + \frac{\bar{\lambda}}{\bar{c}_p} \frac{\partial \tilde{h}_s}{\partial x_j} \right) + \bar{S}_h + \bar{\omega}_h, \quad (4)$$

Energy conservation (~1 eqn)

Reactions  $\sim N^2$   
→ bottle-neck

# The world's 3<sup>rd</sup> most powerful supercomputer: CSC's LUMI in Kajaani



# DLBFoam: open-source code to radically accelerating the chemistry bottle-neck in OpenFOAM CFD simulations

**Solution:** We developed DLBFoam: finite rate chemistry code with Dynamic Load Balancing in order to accelerate the chemistry. Utilizes analytical Jacobian evaluation via pyJac.

**pyJac:** <https://slackha.github.io/pyJac/>

**DLBFoam:** <https://github.com/Aalto-CFD/DLBFoam>

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Computer Physics Communications

[www.elsevier.com/locate/cpc](http://www.elsevier.com/locate/cpc)

DLBFoam: An open-source dynamic load balancing model for fast reacting flow simulations in OpenFOAM <sup>☆,☆☆</sup>

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Physics of Fluids

TUTORIAL

[scitation.org/journal/phf](https://scitation.org/journal/phf)

## Fast reactive flow simulations using analytical Jacobian and dynamic load balancing in OpenFOAM

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Ilya Morev <sup>a</sup>, Bulut Tekgül, Mahmoud Gadalla, Ali Shahanaghi, Jeevananthan Kannan, Shervin Karimkashi, Ossi Kaario, and Ville Vuorinen

### AFFILIATIONS

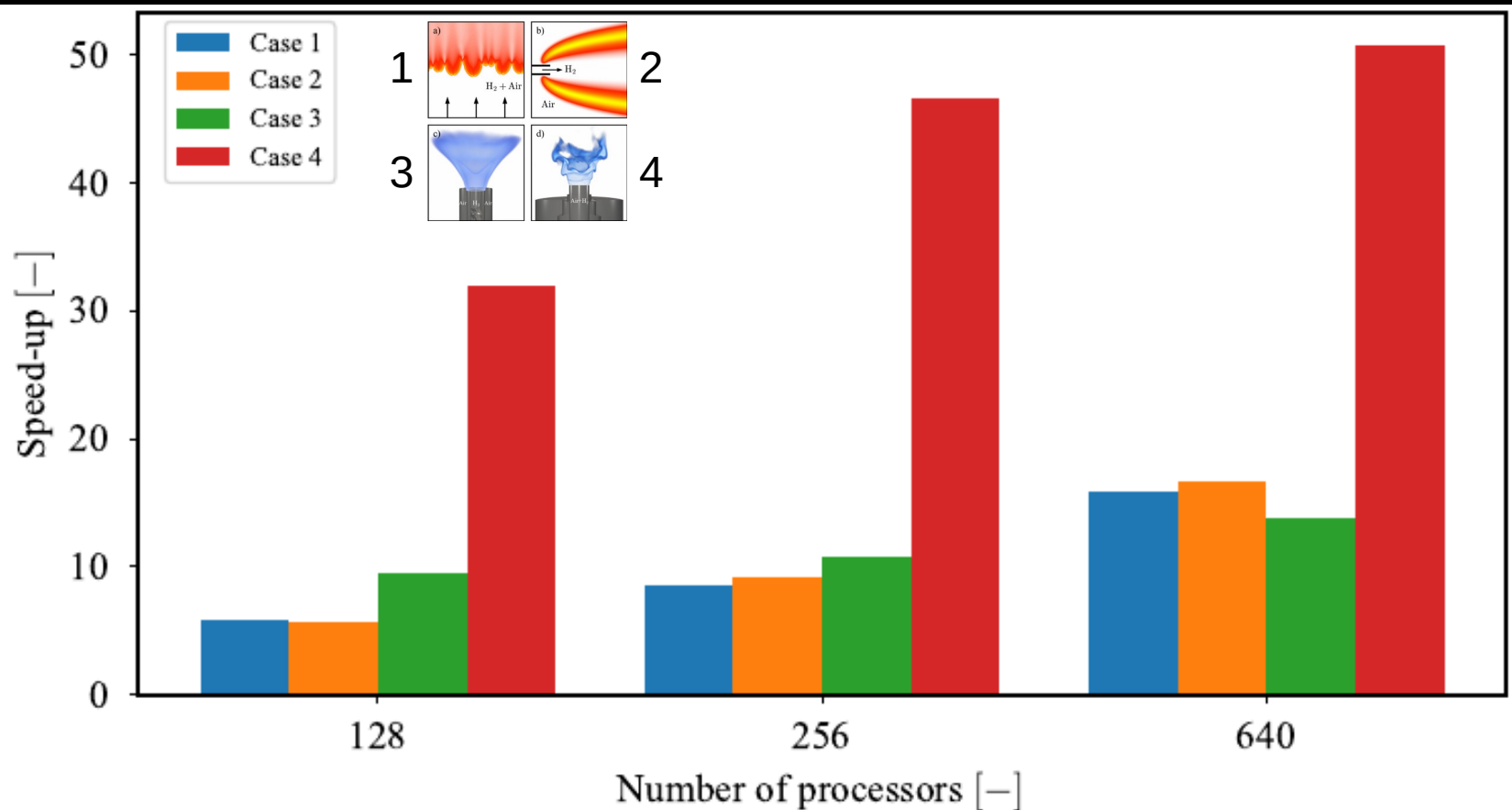
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<sup>a</sup> Author to whom correspondence should be addressed: [ilya.morev@aalto.fi](mailto:ilya.morev@aalto.fi)

# Examples on recent publications where DLBFoam is used

- [1] M.Gadalla, S.Karimkashi, I.Kabil, O.Kaario, T.Lu and V.Vuorinen, Embedded direct numerical simulation of ignition kernel evolution and flame initiation in dual-fuel spray assisted combustion, *Combustion and Flame*, 259, 113172, (2024).
- [2] S.Karimkashi, M.Gadalla, J.Kannan, B.Tekgul, O.Kaario, and V.Vuorinen, Large-eddy simulation of diesel pilot spray ignition in lean methane-air and methanol-air mixtures at different ambient temperatures, *International Journal of Engine Research*, 24, 3, (2023).
- [3] A.Shahanaghi, S.Karimkashi, O.Kaario and V.Vuorinen, Efficient two-dimensional simulation of primary reference fuel ignition under engine-relevant thermal stratification, *Physics of Fluids*, 35, 126102, (2023).
- [4] P.Tamaddonfar, S.Karimkashi, O.Kaario and V.Vuorinen, A Numerical Study on Premixed Turbulent Planar Ammonia/Air and Ammonia/Hydrogen/Air Flames: An Analysis on Flame Displacement Speed and Burning Velocity, *Flow, Turbulence and Combustion*, 111, 717–741, (2023).
- [5] S.Karimkashi, M.Gadalla, J.Kannan, B.Tekgul, O.Kaario, and V.Vuorinen, Large-eddy simulation of diesel pilot spray ignition in lean methane-air and methanol-air mixtures at different ambient temperatures
- [6] B.Tekgul, P.Peltonen, H.Kahila, O.Kaario and V.Vuorinen, DLBFoam: An open-source dynamic load balancing model for fast reacting flow simulations in OpenFOAM, *Computer Physics Communications*, 267, 108073 (2021).
- [7] M.Gadalla, J.Kannan, B.Tekgul, S.Karimkashi, O.Kaario and V.Vuorinen, Large-eddy simulation of tri-fuel combustion Diesel spray assisted ignition of methanol-hydrogen blends, *International Journal of Hydrogen Research*, 46, 41, (2021).
- [8] J.Kannan, M.Gadalla, O.Kaario, S.Karimkashi, B.Tekgul and V.Vuorinen, Large-eddy simulation of tri-fuel ignition diesel spray-assisted ignition of lean hydrogen–methane–air mixtures, *Combustion Theory and Modelling*, 25, 3, (2021).
- [9] B.Tekgul, S.Karimkashi, H.Kahila, Z.Ahmad, J.Hyvönen, E.Lendormy, O.Kaario and V.Vuorinen, Large-eddy simulation of spray assisted dual-fuel ignition under reactivity-controlled dynamic conditions, *FUEL*, 293, 120295, (2021).
- [10] B.Tekgul, V.Vuorinen et al. Large-eddy simulation of dual-fuel spray ignition at different ambient temperatures, *Combustion and Flame*, 215, (2020).
- [11] S.Karimkashi, H.Kahila, O.Kaario, M.Larmi, and V.Vuorinen, A numerical study on combustion mode characterization for locally stratified dual-fuel mixtures, *Combustion and Flame*, 214, (2020).
- [12] H.Kahila, Z.Ahmad, O.Kaario, M.Ghaderi-Masouleh, M.Larmi, and V.Vuorinen, Large-eddy simulation of dual-fuel ignition: Diesel spray injection into a lean methane-air mixture, *Combustion and Flame*, 191, 142-159, (2019).

# DLBFoam: computational speed-up for $H_2$ for 4 different flame cases 1-4 (~5-50x speed-up)



### 3) Remarks about hydrogen

## Oversimplification:



“Hydrogen + Oxygen → Water”



# Hydrogen combustion is complex and also produces **nitric oxide** emissions

E.g. Westbrook et al. (2004)  
 → 19 chemical reactions  
 → 11 molecule species

O'Connor, M., H. J. Curran, J. M. Simmie, W. J. Pitz, and C. K. Westbrook,  
 "A Comprehensive Modeling Study of Hydrogen Oxidation,"  
 Int. J. Chem. Kinet., 36:603-622, 2004 (UCRL-JC-152569).

	Reaction	$A$	$n$	$E_a$	Ref.
H <sub>2</sub> /O <sub>2</sub> Chain Reactions					
1	$\dot{\text{H}} + \text{O}_2 = \dot{\text{O}} + \dot{\text{O}}\text{H}$	$1.91 \times 10^{14}$	0.00	16.44	[39]
2	$\dot{\text{O}} + \text{H}_2 = \dot{\text{H}} + \dot{\text{O}}\text{H}$	$5.08 \times 10^4$	2.67	6.292	[40]
3	$\dot{\text{O}}\text{H} + \text{H}_2 = \dot{\text{H}} + \text{H}_2\text{O}$	$2.16 \times 10^8$	1.51	3.43	[41]
4	$\dot{\text{O}} + \text{H}_2\text{O} = \dot{\text{O}}\text{H} + \dot{\text{O}}\text{H}$	$2.97 \times 10^6$	2.02	13.4	[42]
H <sub>2</sub> /O <sub>2</sub> Dissociation/Recombination Reactions					
5 <sup>a</sup>	$\text{H}_2 + \text{M} = \dot{\text{H}} + \dot{\text{H}} + \text{M}$	$4.57 \times 10^{19}$	-1.40	105.1	[43]
6 <sup>b</sup>	$\dot{\text{O}} + \dot{\text{O}} + \text{M} = \text{O}_2 + \text{M}$	$6.17 \times 10^{15}$	-0.50	0.00	[43]
7 <sup>c</sup>	$\dot{\text{O}} + \dot{\text{H}} + \text{M} = \text{OH} + \text{M}$	$4.72 \times 10^{18}$	-1.00	0.00	[43]
8 <sup>d,e</sup>	$\dot{\text{H}} + \dot{\text{O}}\text{H} + \text{M} = \text{H}_2\text{O} + \text{M}$	$4.50 \times 10^{22}$	-2.00	0.00	[43] × 2.0
Formation and consumption of HO <sub>2</sub>					
9 <sup>f,g</sup>	$\dot{\text{H}} + \text{O}_2 + \text{M} = \text{HO}_2 + \text{M}$	$3.48 \times 10^{16}$	-0.41	-1.12	[44]
	$\dot{\text{H}} + \text{O}_2 = \text{HO}_2$	$1.48 \times 10^{12}$	0.60	0.00	[45]
10	$\text{HO}_2 + \dot{\text{H}} = \text{H}_2 + \text{O}_2$	$1.66 \times 10^{13}$	0.00	0.82	[6]
11	$\text{HO}_2 + \dot{\text{H}} = \dot{\text{O}}\text{H} + \dot{\text{O}}\text{H}$	$7.08 \times 10^{13}$	0.00	0.30	[6]
12	$\text{HO}_2 + \dot{\text{O}} = \dot{\text{O}}\text{H} + \text{O}_2$	$3.25 \times 10^{13}$	0.00	0.00	[46]
13	$\text{HO}_2 + \dot{\text{O}}\text{H} = \text{H}_2\text{O} + \text{O}_2$	$2.89 \times 10^{13}$	0.00	-0.50	[46]
Formation and Consumption of H <sub>2</sub> O <sub>2</sub>					
14 <sup>h</sup>	$\text{HO}_2 + \text{HO}_2 = \text{H}_2\text{O}_2 + \text{O}_2$	$4.2 \times 10^{14}$	0.00	11.98	[47]
	$\text{HO}_2 + \text{HO}_2 = \text{H}_2\text{O}_2 + \text{O}_2$	$1.3 \times 10^{11}$	0.00	-1.629	[47]
15 <sup>i,f</sup>	$\text{H}_2\text{O}_2 + \text{M} = \dot{\text{O}}\text{H} + \dot{\text{O}}\text{H} + \text{M}$	$1.27 \times 10^{17}$	0.00	45.5	[48]
	$\text{H}_2\text{O}_2 = \dot{\text{O}}\text{H} + \dot{\text{O}}\text{H}$	$2.95 \times 10^{14}$	0.00	48.4	[49]
16	$\text{H}_2\text{O}_2 + \dot{\text{H}} = \text{H}_2\text{O} + \dot{\text{O}}\text{H}$	$2.41 \times 10^{13}$	0.00	3.97	[43]
17	$\text{H}_2\text{O}_2 + \dot{\text{H}} = \text{H}_2 + \text{HO}_2$	$6.03 \times 10^{13}$	0.00	7.95	[43] × 1.25
18	$\text{H}_2\text{O}_2 + \dot{\text{O}} = \dot{\text{O}}\text{H} + \text{HO}_2$	$9.55 \times 10^6$	2.00	3.97	[43]
19 <sup>h</sup>	$\text{H}_2\text{O}_2 + \dot{\text{O}}\text{H} = \text{H}_2\text{O} + \text{HO}_2$	$1.0 \times 10^{12}$	0.00	0.00	[50]
	$\text{H}_2\text{O}_2 + \dot{\text{O}}\text{H} = \text{H}_2\text{O} + \text{HO}_2$	$5.8 \times 10^{14}$	0.00	9.56	[50]

Hydrogen is actually quite different from other fuels.  
Not only diffusive/light but also very high flame speed.

Hydrogen ( $\text{H}_2$ ) has very different combustion properties when compared to hydrocarbons e.g. methane ( $\text{CH}_4$ ) or propane ( $\text{C}_3\text{H}_8$ )

Table 1

Thermal properties and fundamental combustion characteristics of ammonia and hydrocarbon fuels. Data of boiling point and condensation point are from NIST database [8].

Fuel	$\text{NH}_3$	$\text{H}_2$	$\text{CH}_4$	$\text{C}_3\text{H}_8$
Boiling temperature at 1 atm ( $^{\circ}\text{C}$ )	-33.4	-253	-161	-42.1
Condensation pressure at 25 $^{\circ}\text{C}$ (atm)	9.90	N/A	N/A	9.40
Lower heating value, LHV (MJ/kg)	18.6	120	50.0	46.4
Flammability limit (Equivalence ratio)	0.63~1.40	0.10~7.1	0.50~1.7	0.51~2.5
Adiabatic flame temperature ( $^{\circ}\text{C}$ )	1800	2110	1950	2000
Maximum laminar burning velocity (m/s)	0.07	2.91	0.37	0.43
Minimum auto ignition temperature ( $^{\circ}\text{C}$ )	650	520	630	450

Flame speed is very important concept affecting fluid dynamical design of combustion devices.

E.g. try to avoid “flashback” vs “blow-out”

# Simulated premixed $H_2$ combustion/AHEAD burner

To be submitted

Courtesy:  
A.Haider/  
Aalto



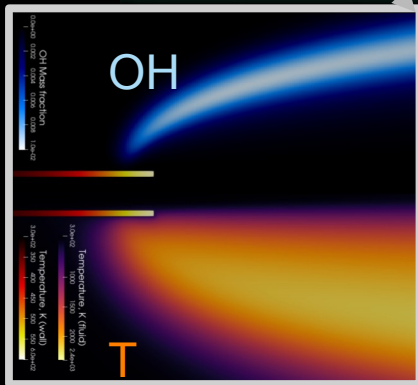
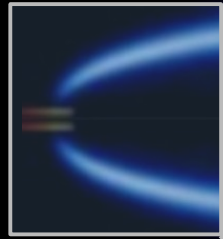
# How do you know your simulation is correct?

→ Compare 3D flame structure sim. vs exp.

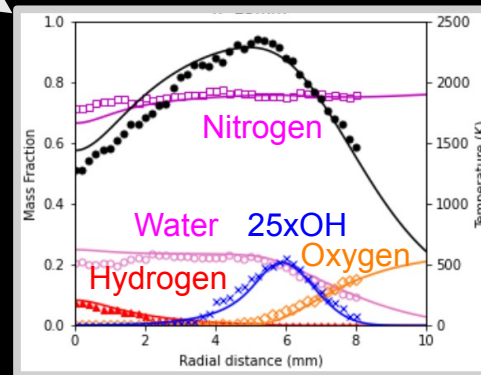
“Case 2”: Simulated  $H_2$  jet flame (steady)

I. Morev

OH



Zoom to  
injector



Experiment vs  
simulation

## 4) Aalto/ENG + international efforts to model hydrogen flames

## TNF Workshop

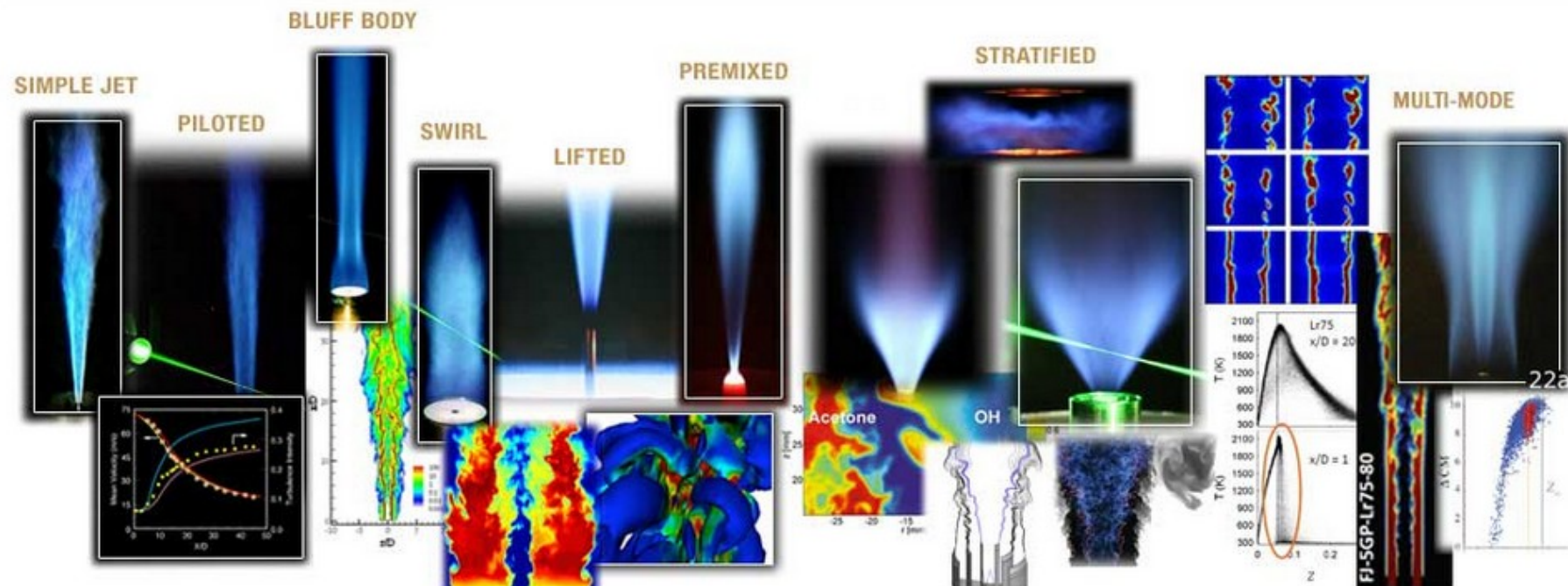
International Workshop on Measurement and Computation of Turbulent Flames

**HOME**

DATA ARCHIVES

WORKSHOP PROCEEDINGS

## CONTACT



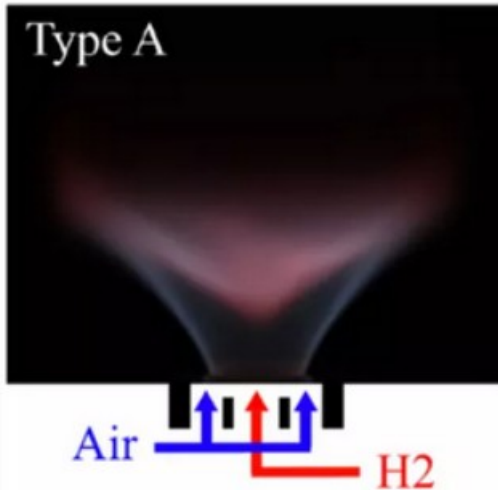


# May 2023: International initiative to compare different CFD codes against high quality experimental data on three hydrogen flame rigs

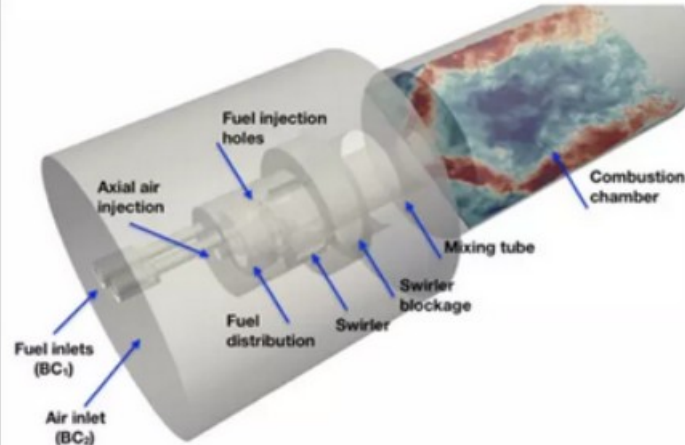
## Clean Aviation working group on CFD codes for hydrogen-air combustion

Experimental, high-precision data will be made available from **three experiments**: the **HYLON rig** in Toulouse, the **TU Berlin rig** in Berlin and the **NTNU rig** in Trondheim. Only pure hydrogen-air flames will be considered in the frame of this workshop.

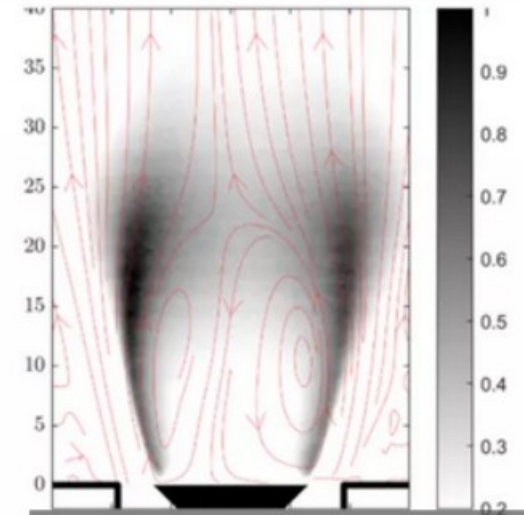
### TOULOUSE RIG



### BERLIN RIG

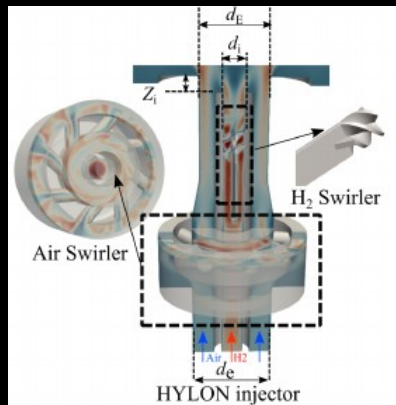


### NTNU RIG

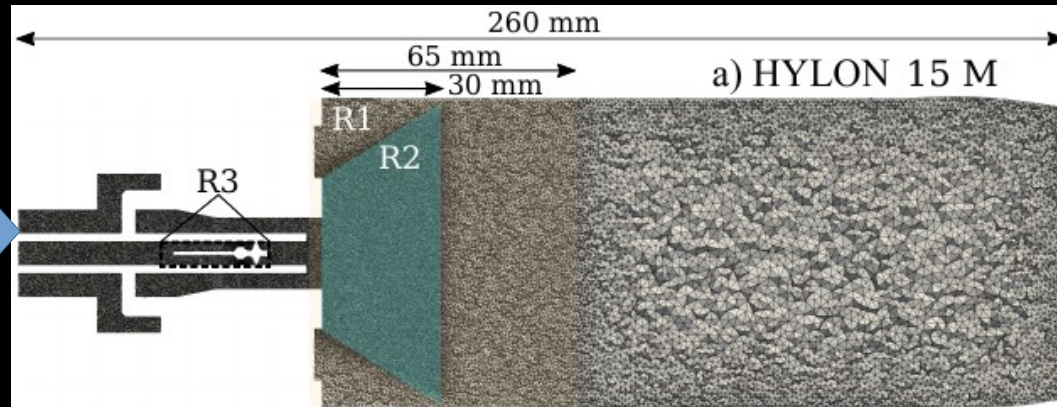


# Computational modeling steps before H<sub>2</sub> flame CFD simulations

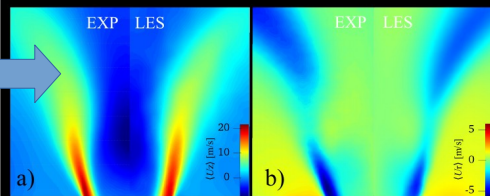
## Step 1: 3D CAD model



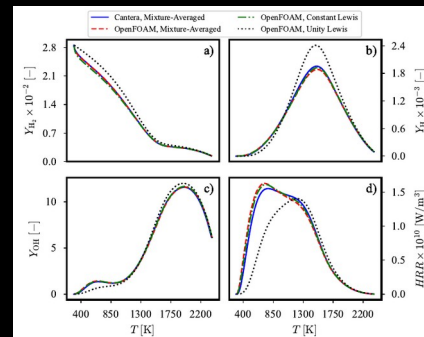
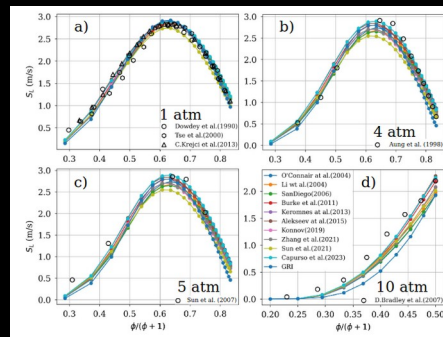
## Step 2: 3D meshing



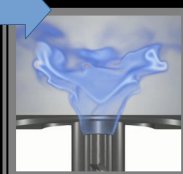
## Step 3: Cold flow validation (3d)



## Step 4: Chemistry+diffusion validation/verification (0d/1d)

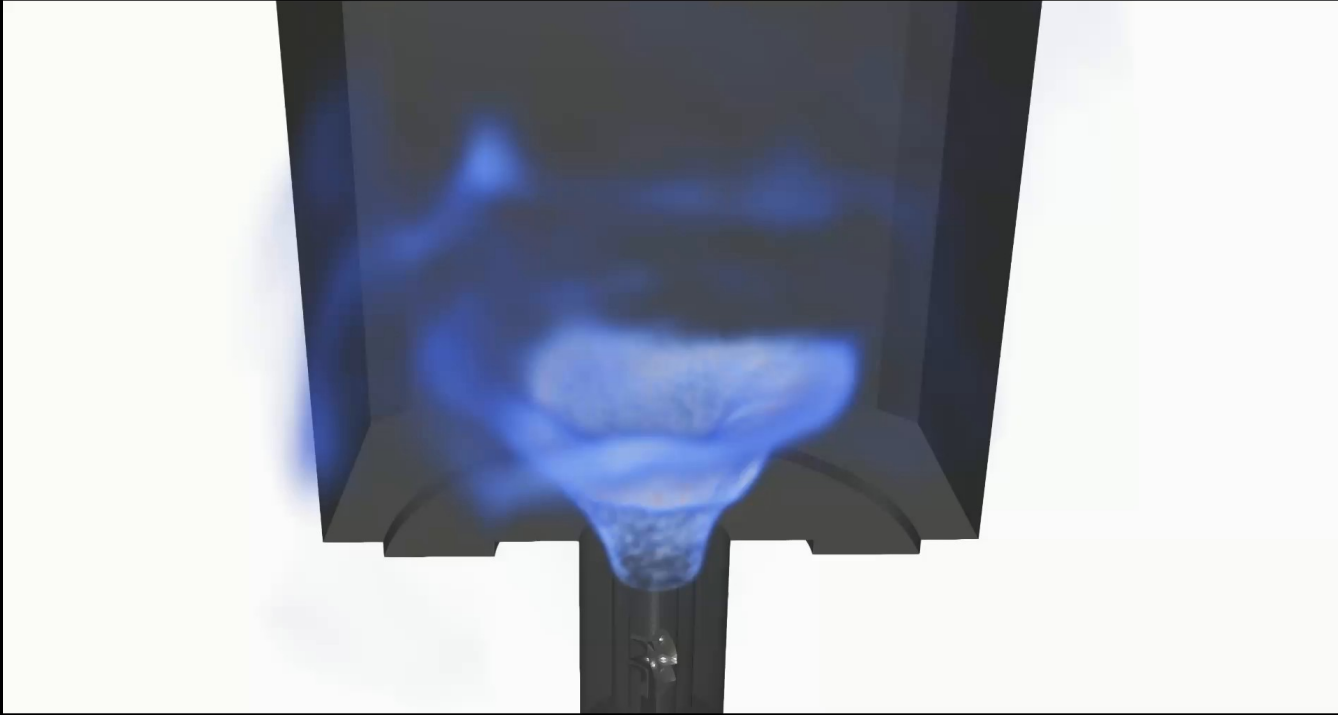


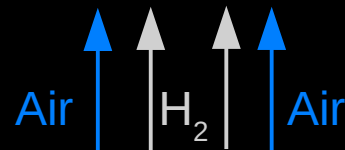
## Step 5: Reactive flow (3d)



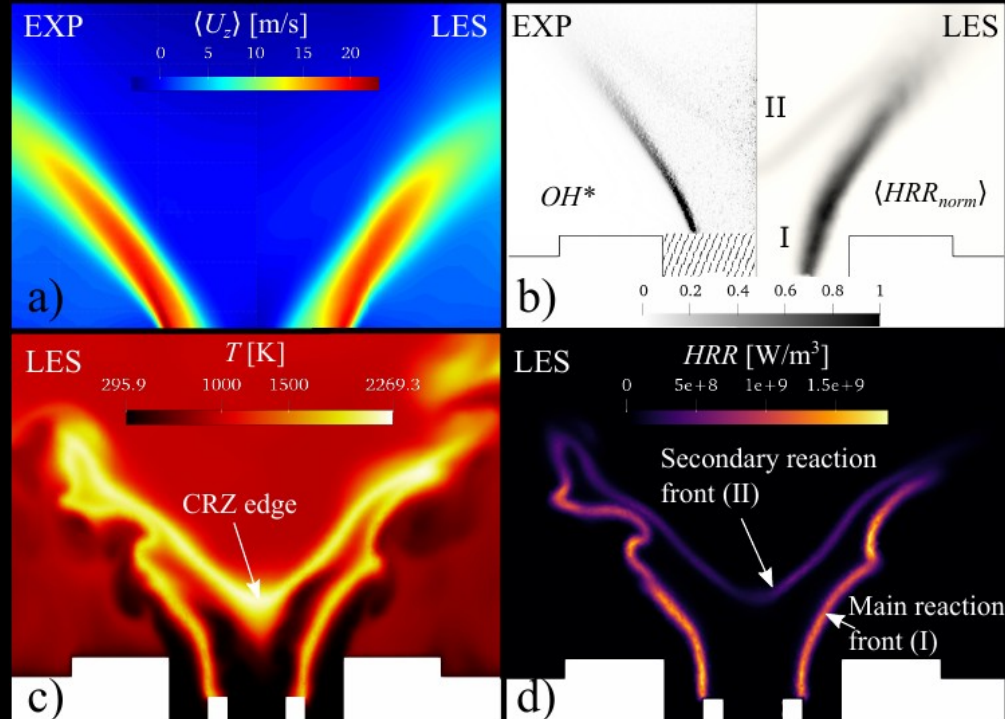
# Large-eddy simulation of HYLON Flame A setup (TOULOUSE rig): non-premixed hydrogen combustion

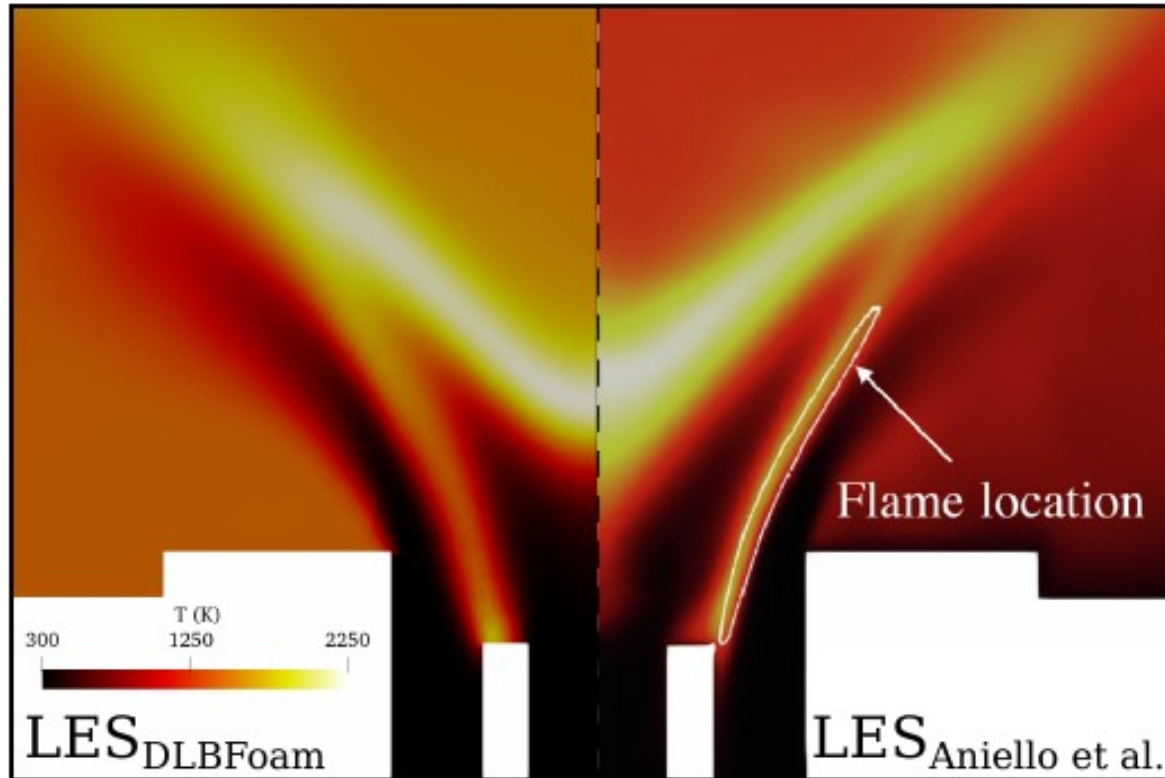
Courtesy: Z.Shahin (M.Sc. thesis 2023)





# HYLON Flame A: comparison of present simulation (LES/CFD) against experimental data

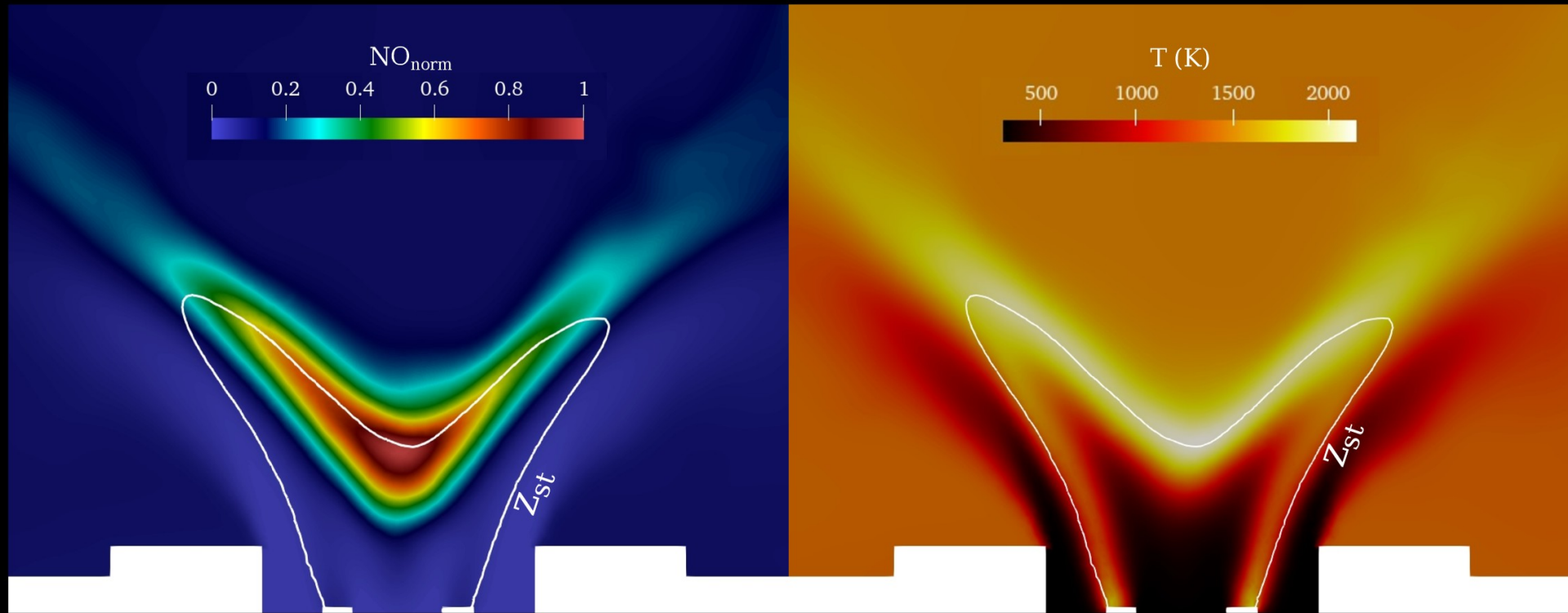




**Figure 36:** Contour map of the the temperature observed from the current work a) and the LES values from [14]b) for the anchored flame A.



# NO<sub>x</sub> emissions vs local temperature



Courtesy: Z.Shahin (M.Sc. thesis 2023)

## 5) Concluding remarks



# Personal experiences from our team on solving very difficult computational problems

- 1) show that it is possible to solve a problem
- 2) do it more efficiently
- 3) make your code/setups open to everyone
- 4) trust on the power of community efforts e.g. “OpenFOAM”
- 5) go back to 1)

*“Simulation has become the third scientific pillar alongside theory and experiments”* (Prof. C.Hasse/Nov. 6<sup>th</sup> 2023)

$$\frac{\partial u_i}{\partial t} + \frac{\partial u_j u_i}{\partial x_j} = - \frac{\partial p}{\partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_j^2}$$



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